6.3 Signal Space Concepts

As in the case of vectors, we now develop a parallel treatment for a set of signals.

Definition 6.34.

(a) The **inner product** of two real-valued signals $x_1(t)$ and $x_2(t)$ is denoted by $\langle x_1(t), x_2(t) \rangle$ and defined by

$$\langle x_1(t), x_2(t) \rangle = \int_{-\infty}^{\infty} x_1(t) x_2(t) dt.$$

- (b) The signals are **orthogonal** if their inner product is zero.
- (c) The **norm** of a signal is defined as

$$||x(t)|| = \sqrt{\langle x(t), x(t) \rangle} = \sqrt{E_x}$$

where E_x is the energy in x(t):

$$\langle x(t), x(t) \rangle = \int_{-\infty}^{\infty} |x(t)|^2 dt \equiv E_x$$

(d) A collection of N signals is **orthonormal** if the signals are orthogonal and their norms are all unity.

Example 6.35. Consider the two waveforms shown in Figure 16.

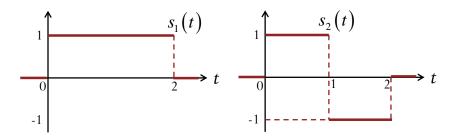


Figure 16: Two Waveforms in Example 6.35

Definition 6.36.

(a) The **projection** of $x_2(t)$ to $x_1(t)$ is given by

$$\operatorname{proj}_{x_{1}(t)}x_{2}(t) = \frac{\langle x_{2}(t), x_{1}(t) \rangle}{\langle x_{1}(t), x_{1}(t) \rangle} x_{1}(t) = \frac{\langle x_{2}(t), x_{1}(t) \rangle}{E_{x_{1}}} x_{1}(t)$$

(b) The **cross-correlation coefficient** of $x_1(t)$ and $x_2(t)$ is defined as

$$\rho_{x_1,x_2} = \frac{\langle x_1(t), x_2(t) \rangle}{\sqrt{E_{x_1}E_{x_2}}}.$$

•
$$\operatorname{proj}_{x_1(t)} x_2(t) = \sqrt{E_{x_2}} \rho_{x_2, x_1} \frac{x_1(t)}{\sqrt{E_{x_1}}}$$

Example 6.37. For the two waveforms shown in Figure 16,

6.38. Similar to 6.30, the Gram-Schmidt Orthogonalization Procedure (GSOP) can be used to construct a set of orthonormal waveforms from a set of finite energy signal waveforms: $\{s_j(t), j = 1, 2, ..., M\}$.

The first orthonormal function is simply constructed as

$$\phi_1(t) = \frac{u_1(t)}{\sqrt{E_{u_1}}} = \frac{s_1(t)}{\sqrt{E_{s_1}}}.$$

The subsequent orthonormal functions are found as follows:

$$\phi_i(t) = \frac{u_i(t)}{\sqrt{E_{u_i}}},$$

where the unnormalized basis function $u_i(t)$ is given by

$$u_i(t) = s_i(t) - \sum_{k=1}^{i-1} \text{proj}_{u_k(t)} s_i(t).$$

and

$$\operatorname{proj}_{u_{k}(t)} s_{i}\left(t\right) = \frac{\left\langle s_{i}\left(t\right), u_{k}\left(t\right)\right\rangle}{\left\langle u_{k}\left(t\right), u_{k}\left(t\right)\right\rangle} u_{k}\left(t\right) = \left\langle s_{i}\left(t\right), \phi_{k}\left(t\right)\right\rangle \phi_{k}\left(t\right)$$

As with the GSOP for vectors, we also discard the zero functions. In general, the final number of orthonormal functions, N, is less than or equal to the number of given waveforms, M, depending on one of the two possibilities:

- (a) If the waveforms $\{s_j(t), j = 1, 2, ..., M\}$ form a linearly independent set, then N = M.
- (b) If the waveforms $\{s_j(t), j = 1, 2, ..., M\}$ are not linearly independent, then N < M.

Example 6.39. Consider the four waveforms illustrated in Figure 17. <u>Use</u> the Gram-Schmidt orthogonalization procedure (where the waveforms are applied in the order given) to find the orthonormal basis waveforms $\phi_1(t)$, $\phi_2(t)$, ... whose linear combinations can be used to represent the four waveforms.

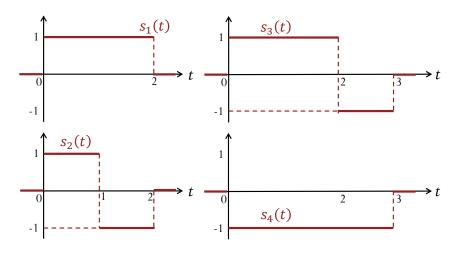


Figure 17: Four signals for orthogonalization in Example 6.39

• First we set $u_1(t) = s_1(t)$.

$$E_{u_1} = E_{s_1} = \phi_1(t) = \frac{u_1(t)}{\sqrt{E_{u_1}}} = \frac{s_1(t)}{\sqrt{E_{s_1}}} =$$

• $u_2(t) = s_2(t) - \text{proj}_{u_1} s_2 =$

$$E_{u_2} = \phi_2(t) = \frac{u_2(t)}{\sqrt{E_{u_2}}} =$$

•
$$u_3(t) = s_3(t) - \text{proj}_{u_1} s_3 - \text{proj}_{u_2} s_3$$

$$E_{u_3} = \phi_3(t) = \frac{u_3(t)}{\sqrt{E_{u_3}}} =$$

• $u_4(t) = s_4(t) - \text{proj}_{u_1} s_4 - \text{proj}_{u_2} s_4 - \text{proj}_{u_1} s_4 - \text{proj}_{u_3} s_4$

6.40. Once we have constructed¹⁵ the set of, say N, orthonormal waveforms $\{\phi_i(t), i = 1, 2, ..., N\}$, we can express the signals $s_i(t)$ as linear combinations of the N orthonormal basis functions $\phi_i(t)$. Thus, we may write

$$s_j(t) = \sum_{i=1}^{N} s_i^{(j)} \phi_i(t)$$
 (34)

where the constants (weights)

$$s_i^{(j)} = \langle s_j(t), \phi_i(t) \rangle. \tag{35}$$

¹⁵We have shown how this set can be constructed from GSOP. However, in practice, this set may be derived from different procedure.

Note that $s_i^{(j)}\phi_i(t) = \langle s_j(t), \phi_i(t) \rangle \phi_i(t)$ can be geometrically interpreted as the projection of the signal $s_j(t)$ onto the *i*th axis, $\phi_i(t)$.

Based on (34), each signal may be represented by the vector (or sequence)

$$\mathbf{s}^{(j)} = (s_1^{(j)}, s_2^{(j)}, \dots, s_N^{(j)})^T, \tag{36}$$

or, equivalently, as a point in the N-dimensional (in general, complex) signal space.

The (mathematical/conceptual) conversion/mapping from waveform to it corresponding vector in (36) and (35) is shown in Figure 18a. The inverse mapping from vector to waveform in (34) is shown in Figure 18b.

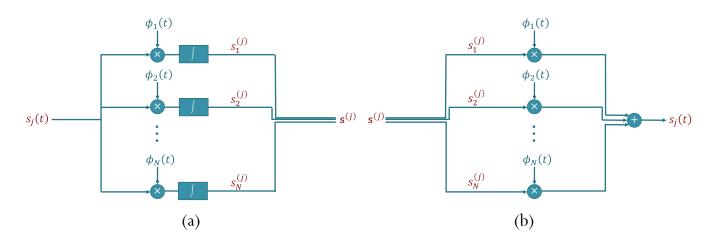


Figure 18: Waveform to vector (a), and vector to waveform (b) mappings.

Example 6.41. For the four waveforms in Example 6.39 and the orthonormal basis derived from GSOP,